AMENDMENTS TO THE SPECIFICATION

Please replace the paragraph on pg. 2, ll. 3 – 9 with the following:

The AGC measurements required for flow control under the TIA/EIA/IS-856 standard are analog in nature and noisy. Therefore, AGC measurements must be low pass filtered in order to enhance their reliability. The time constant for low pass filtering ~~sheltering~~ is typically in the order of 1.28 seconds. Thus, low pass filtering introduces delay in the generation of reverse link loading estimates, which, in turn, increases the response time of the base station to changes in reverse link loading. The longer response time means that the base station may not be able to track fast changes in reverse link loading and may, therefore, be ineffective under such conditions.

Please replace the paragraph on pg. 6, ll. 8 – 13 with the following:

Network 10 as illustrated comprises a plurality of sectors 12, each served by a radio base station (RBS) [[12]]14, a base station controller (BSC) [[16]]14 supporting the RBSs 12, a mobile switching center (MSC) 18 interfacing the network 10 to one or more external networks 20, and a packet data service node (PDSN) 22 interfacing the network 10 to one or more packet data networks 24. Examples of networks 20 and 24 include but are not limited to the Public Switched Telephone Network (PSTN) and the Internet, respectively.

Please replace the paragraph on pg. 8, line 13 to pg. 9, line 2 with the following:

Typically, each RBS [[16]]14 includes one or more receivers for receiving signals transmitted from the terminals 17 on the reverse link. These receivers usually have some form of automatic gain control (AGC) circuit that compensates for changes in the receiver's noise flow caused by changing reverse link interference within the sector 12 in which the RBS [[16]]14 is located. More particularly, AGC circuits typically work to maintain the received signal within a given range to avoid saturation in analog-to-digital conversion of the signal. With conventional

approaches, the AGC circuit control voltage may be used to infer reverse link interference because that voltage is a function of the reverse link interference. In turn reverse link interference is a function of reverse link loading. Thus, the total reverse link interference in a given sector 12 may be used as an indicator of the reverse link loading in that sector. Computing total sector interference for the reverse link using AGC measurements is slow (e.g., < 1 Hz) and inaccurate. The slowness stems for the need to aggressively low-pass filter the measurements due to noise, while the inaccuracy arise from a number of sources, including the dependence of the receiver's noise figure which changes over time.

Please replace the paragraph on pg. 13, ll. 12 – 20 with the following:

The demodulator 34 within interface 32 provides pilot SNR information to the load estimator 42. That is, the demodulator 34 in the i^{th} interface 32 provides pilot SNR information about the i^{th} terminal 17 to the load estimator 42. Those skilled in the art will recognize that pilot SNR determination is a common operation performed by demodulators, particular in code division multiple access (CDMA) receivers. However, in some instances, it may not be convenient to make the pilot SNR information determined within the demodulator 34 available to the load estimator 42. For example, the demodulator [[42]]<u>34</u> is often implemented as an integrated circuit, which may or may not make pilot SNR information externally available in a form suitable for the load estimator 42.